



SPHERE

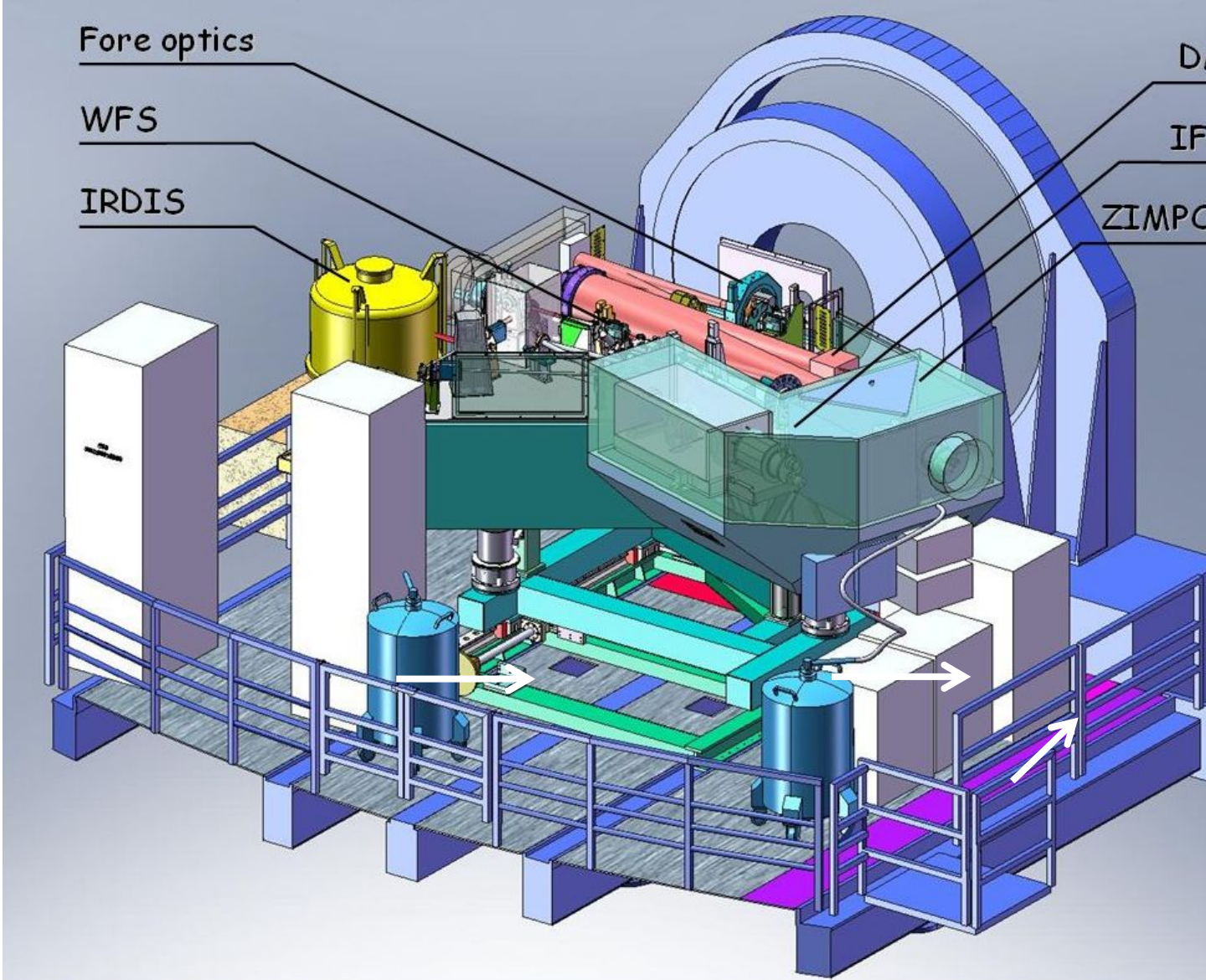
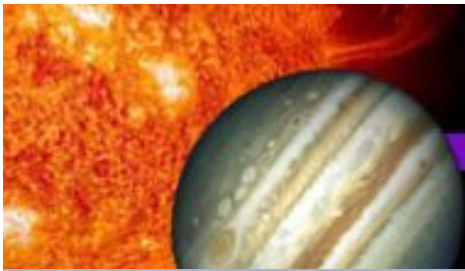
SPHERE:

~~Confronting in-lab performance~~
with system analysis predictions

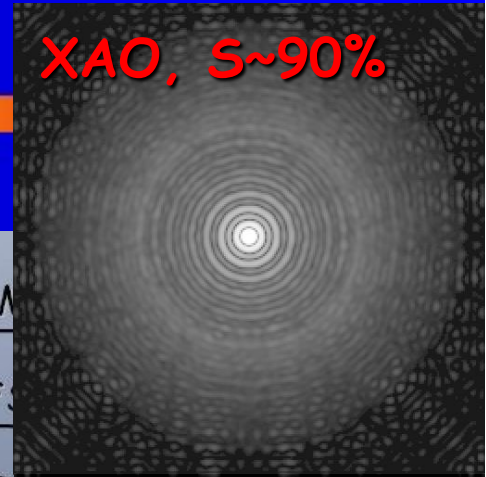


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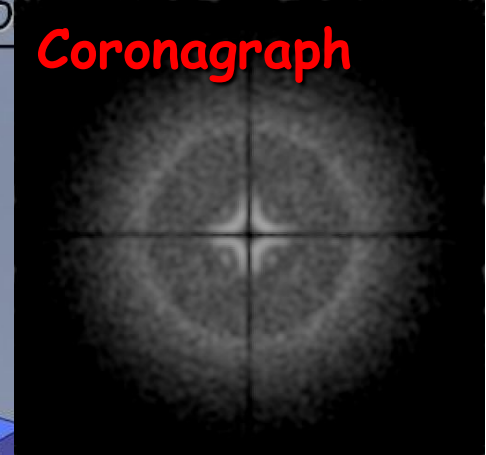
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XAO, $S \sim 90\%$



Coronagraph



Diff. Methods



The slide features a header with a blue background and a rainbow-colored horizontal line. On the left, there is a composite image of the Sun and the planet Jupiter. The title 'SPHERE' is written in large white letters, and 'System overview' is written in yellow below it. The main content is a bulleted list on a black background with white text. The list describes the system's capabilities and limitations.

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System overview

- Integrated system
- Dedicated to high dynamic range imaging
 - Lots of stuff
 - Selectable coronagraphs, Vis and NIR
 - Pupil stabilisation
 - Differential TT control
 - etc
 - But none of the "nice to have" features that classical AO would be tempted to include
 - No field selector
 - No general purpose IR WFS
 - etc

The logo for the SPHERE project features a vibrant background with a blue top section and a rainbow-colored horizontal band. On the left, there is a depiction of the Sun in orange and red, and the planet Jupiter with its characteristic bands. The word "SPHERE" is written in large, white, bold, sans-serif capital letters across the top.

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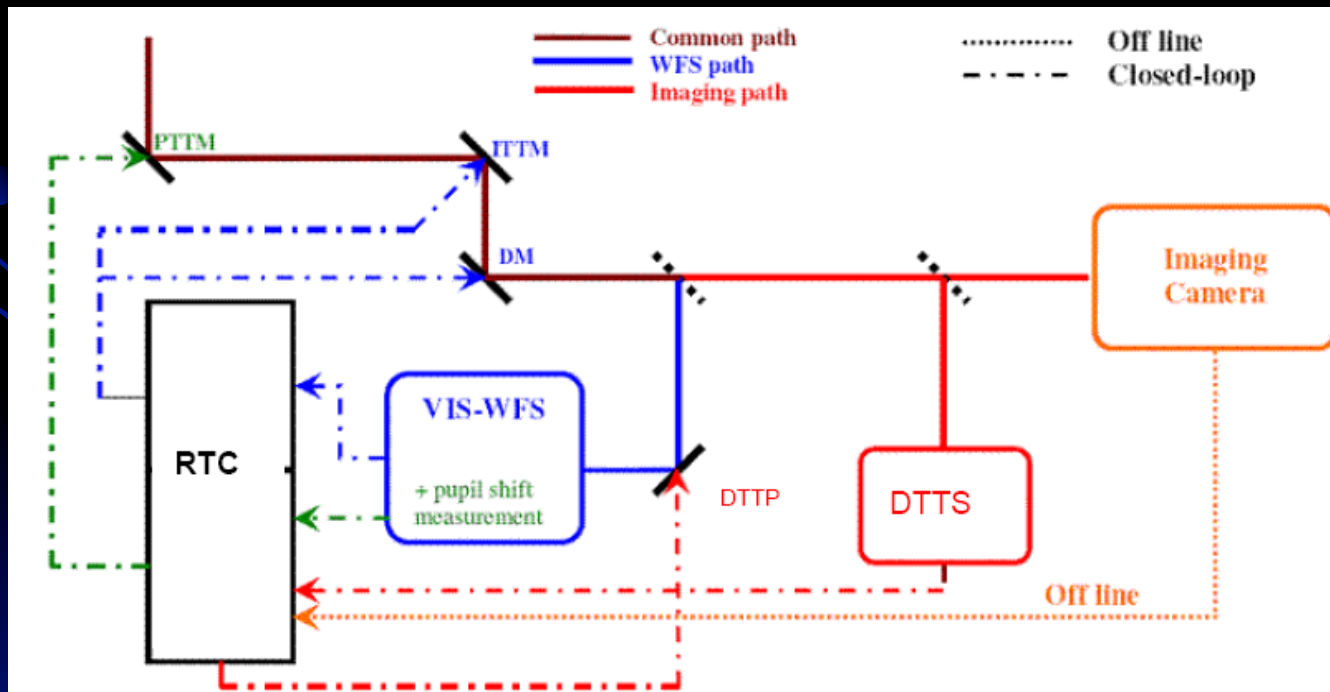
System overview

- Present here some optical aspects of system analysis and performance prediction
 - In reality the system includes far more
 - Tribute to a large group of people working on all aspects, opto-mechanical design and integration to motor control, instrument software, and data reduction
 - Consortium with participants from labs all across Europe, ESO, and several industrial companies
- 
- In the bottom-left corner of the slide, there are decorative blue curved lines that resemble orbital paths or trajectories, with small blue dots placed at various points along these curves.

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Adaptive optics features

- Image stability essential for the coronagraphic PSF
 - Differential atmospheric dispersion
 - Thermo-mechanical drift
- Differential TT sensor implemented
- NCPA calibration
 - Phase Diversity algorithm
 - Minimizes aberrations in the coronagraph plane
 - Corrects at least 55 Zernike modes (up to about $4c/pup$)



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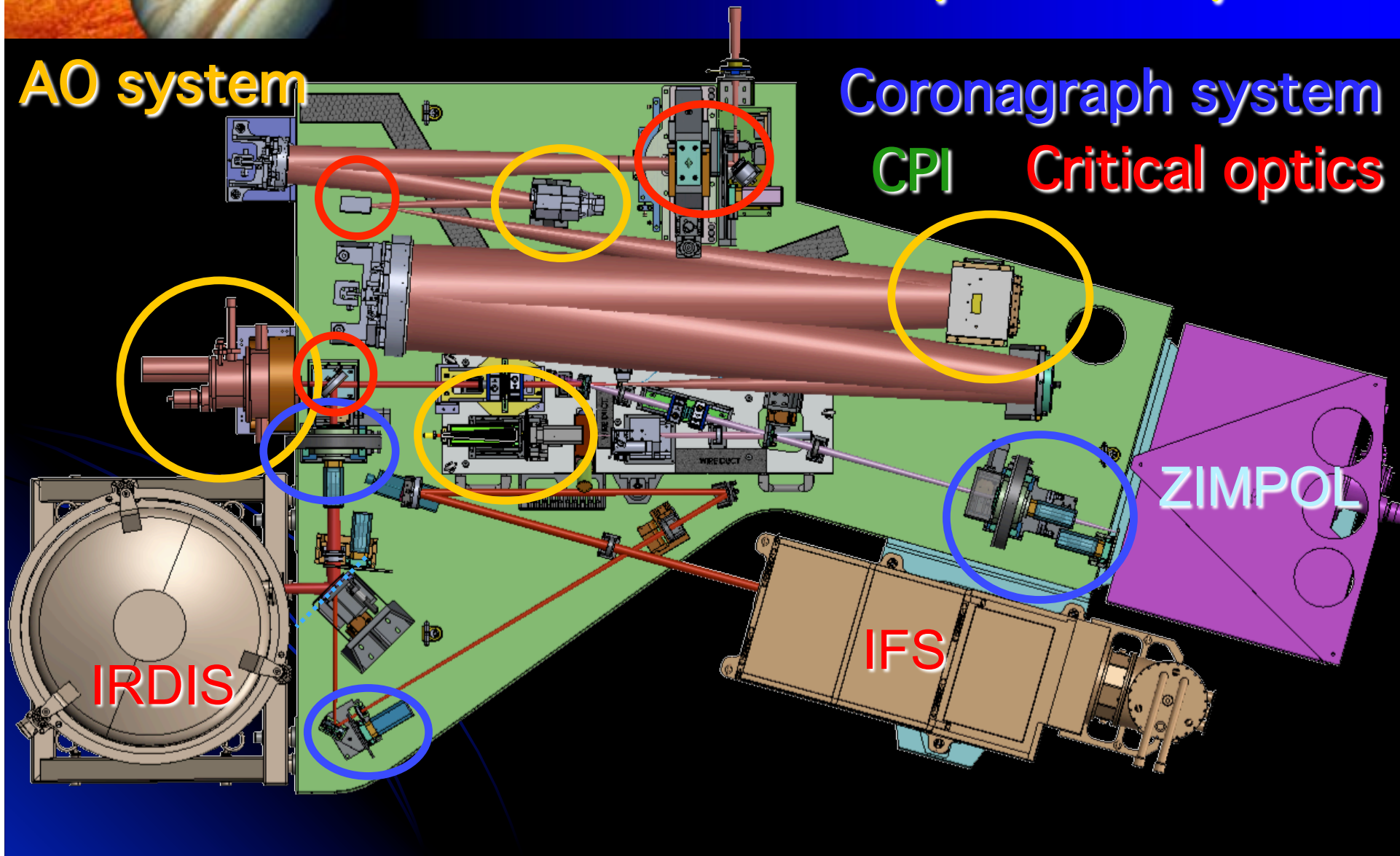
Optical lay-out

AO system

Coronagraph system

CPI

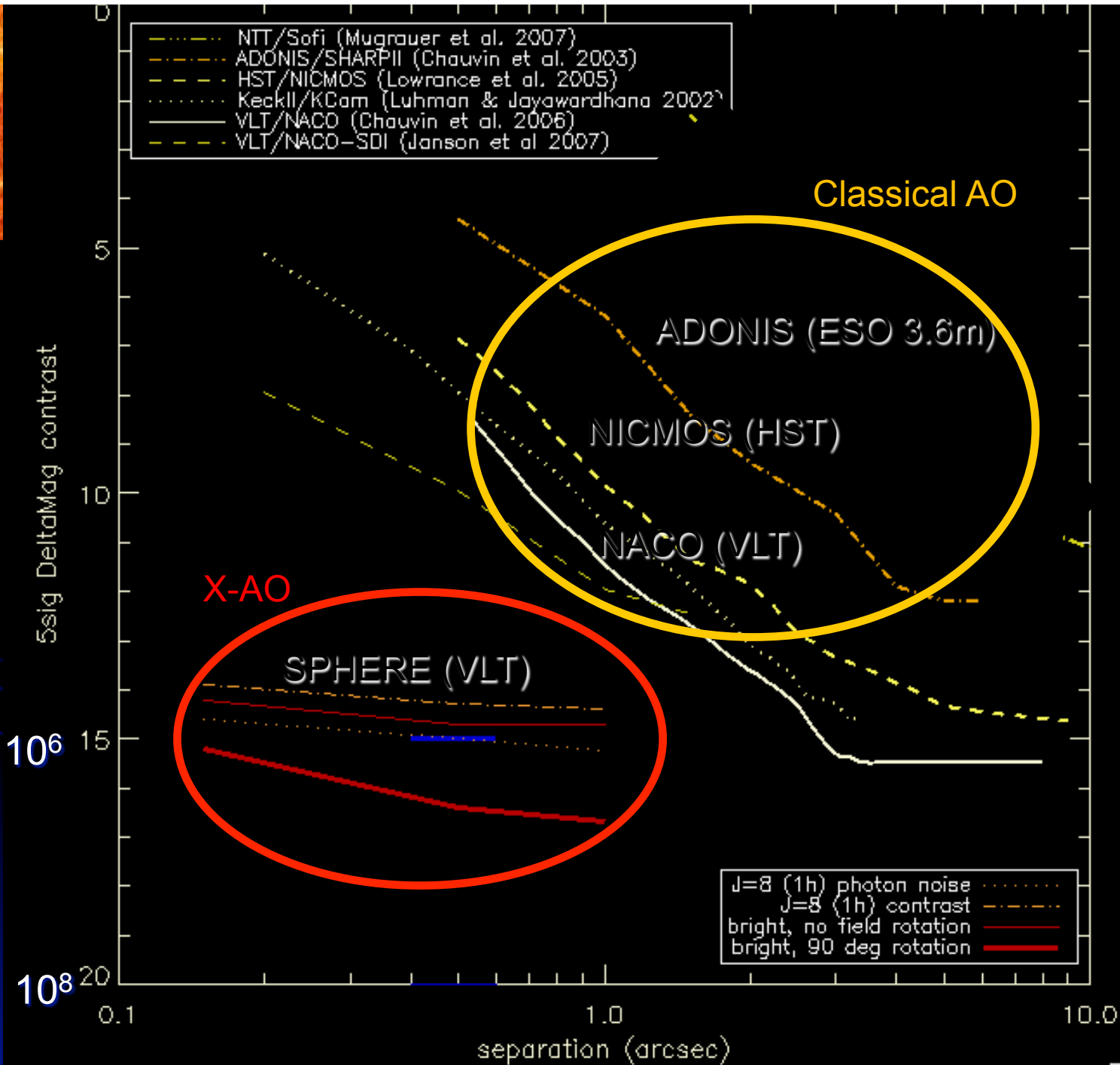
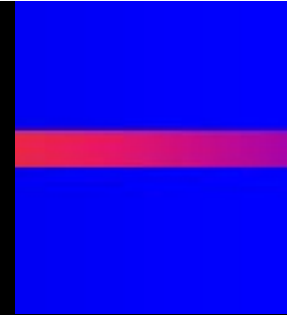
Critical optics



IRDIS

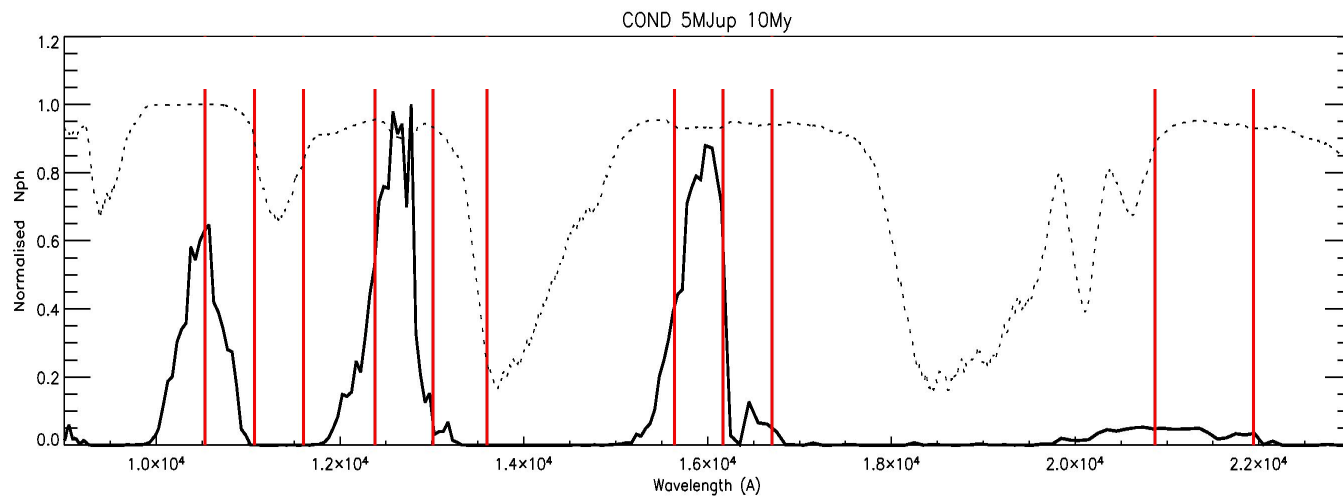
ZIMPOL

IFS



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Spectral differential imaging



- Speckles scale with wavelength but the pattern remains mostly constant
- How constant?
- Which performance criterion?

$5 \cdot 10^{-6}$ ($5 \cdot 10^{-7}$) at $0.5''$

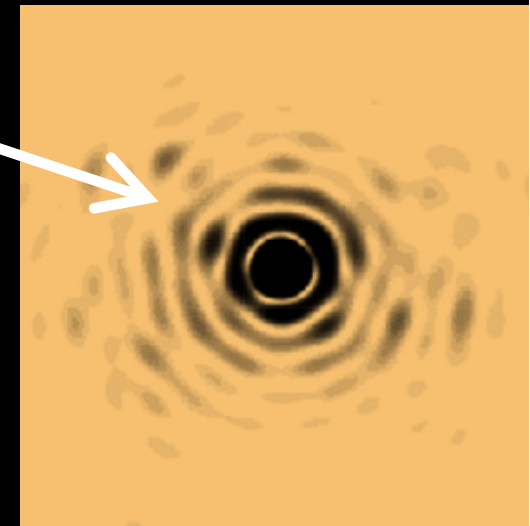
$11'' \times 12.5''$



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Imaging theory: Fraunhofer approximation

- Assuming all optics in the pupil plane
- Image is Fourier transform of the pupil
- For small aberrations, PSF essentially described by three terms
 - The Airy pattern
 - The wavefront Power Spectral Density (PSD)
 - A cross term: Pinned Speckles
- A perfect coronagraph removes the Airy pattern and the Pinned Speckles
- Left with the PSD

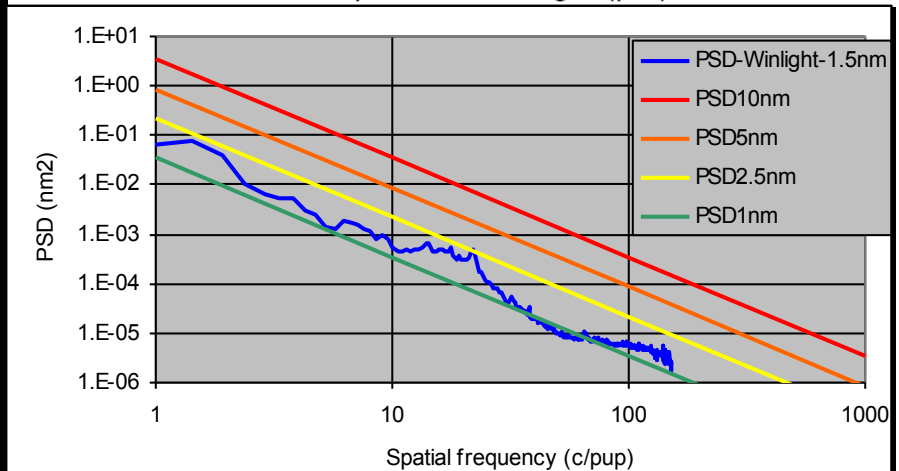
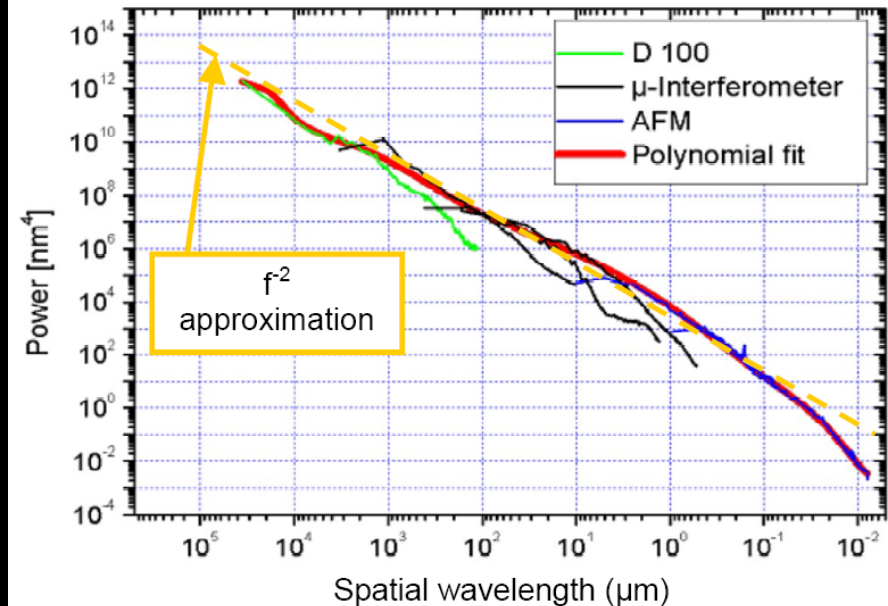


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Optics description: PSD

- Residual speckles \sim PSD
 - Proportional to $(WFERms)^2$
 - Hence related to Strehl ratio...
- PSD characterizes error distribution over spatial frequencies
 - Expected speckle intensity at different points in the FOV
 - Exactly what we need
- But cumbersome to use and difficult to communicate
- Good optics tends to follow a $1/f^2$ - law
 - Use as working assumption and make budget based on WFERms
 - To account for AO correction and NCPA calibration, define three different budgeting bands:

Lo - Mid - Hi





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PSD model vs AO imaging simulation

- Budget considers assumed azimuthally averaged PSDs for each optical surface
- Total budget obtained by summing individual PSDs
- Provides input to an adaptive optics simulator based on CAOS (eg. Carbillet et al 2008)
 - Takes into account instrumental effects that are not described by the simple PSD model
 - Coronagraph decenter, pupil misalignment, atmospheric residuals, etc
- PSD budget allows optical design trade-offs and fixing optics manufacturing specs



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Role of AO in the PSD budget

- AO corrects common-path instrumental aberrations
 - Filter the PSD up to $f_{\text{Mid}} = 20c/\text{pup}$
- But adds non-common path aberrations to the science beam
- Calibrate these aberrations using Phase-Diversity
 - Filter the PSD up to $f_{L_0} = 4c/\text{pup}$
- Calibration is not efficient for time variable aberrations
 - Rotating elements (ADCs)
 - Beam shift effects

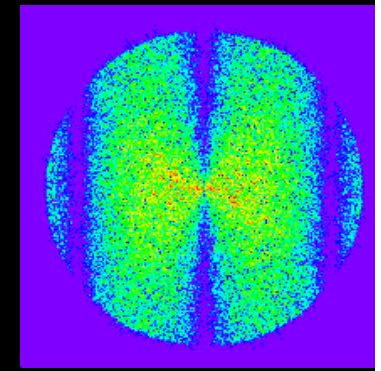
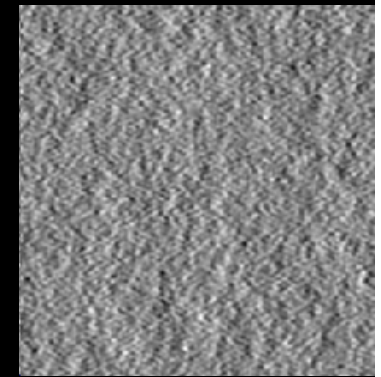
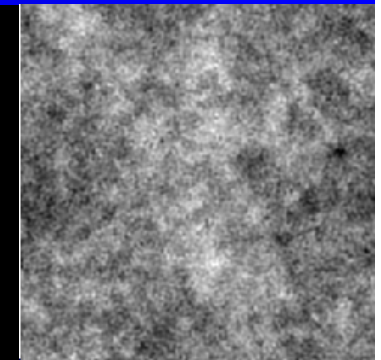
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Out-of-pupil aberrations: Beam shift

- Due to atmospheric dispersion, the visible beam (WFS) does not see the same aberrations as the NIR science beam
- Residual error is the difference between two identical phase screens shifted by a fraction $\delta p/d$
- For spatial frequencies $f \ll \delta p/d$, the PSD of the difference is approximately:

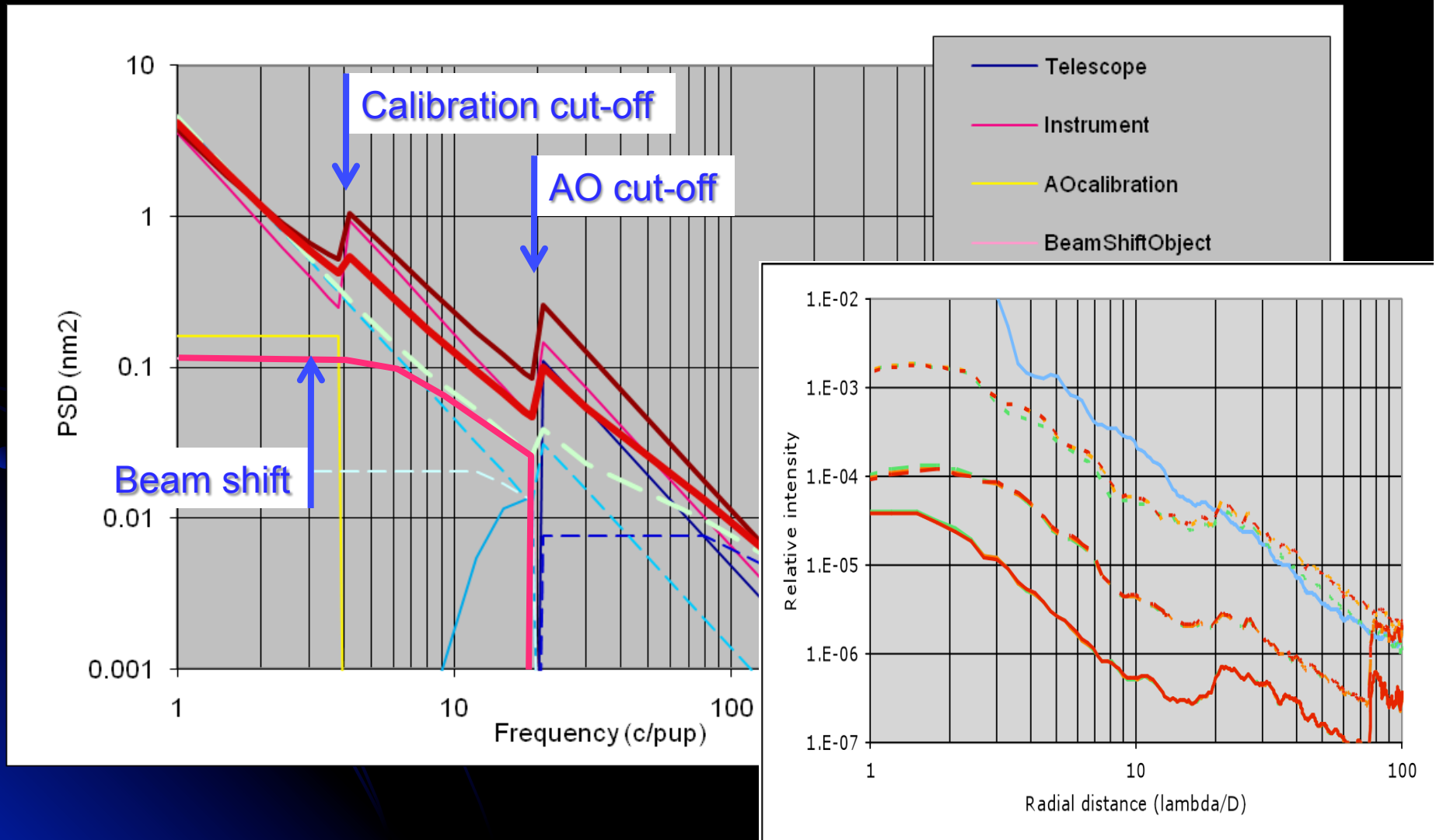
$$\Delta PSD = \left(\frac{2\pi f \delta p}{d} \right)^2 PSD$$

- For our $1/f^2$ model, the result is a constant
- Affects mirrors upstream of the dichroic close to image planes:
 - PTTM, Derotator, TM2
- Budgeting these items allowed to fix minimum out-of-image distances for these optics.



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Resulting PSD budget





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Differential aberrations

- What is the residual after spectral differential imaging?
 - Chromatic speckle evolution
 - Higher order PSF terms
 - Differential aberrations between imaging channels (Cavarroc 2006)

$$\Delta I \propto PSD_{Fore} \sigma_{Diff}$$

- Introduces differential aberrations as important parameter in the budget
- Good balance of various effects is found with WFE_{diff} = 10nm
 - Set as spec for IRDIS
- Nearly negligible effect found for WFE_{diff} = 5nm
 - Set as goal
- **As-built budget indicates that we are very close to goal**
- Confirmed by Phase diversity measurements

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Out-of-pupil aberrations: Fresnel effect

- Treated by Marois et al in 2006
 - Propagation to the pupil plane transforms phase errors into amplitude according to Talbot
 - Depends on wavelength and spatial frequency
- Note that in the case of an ideal coronagraph, an out-of-pupil phase screen alone is OK
- Problem is that a cross term appears when mixing with an in-pupil screen

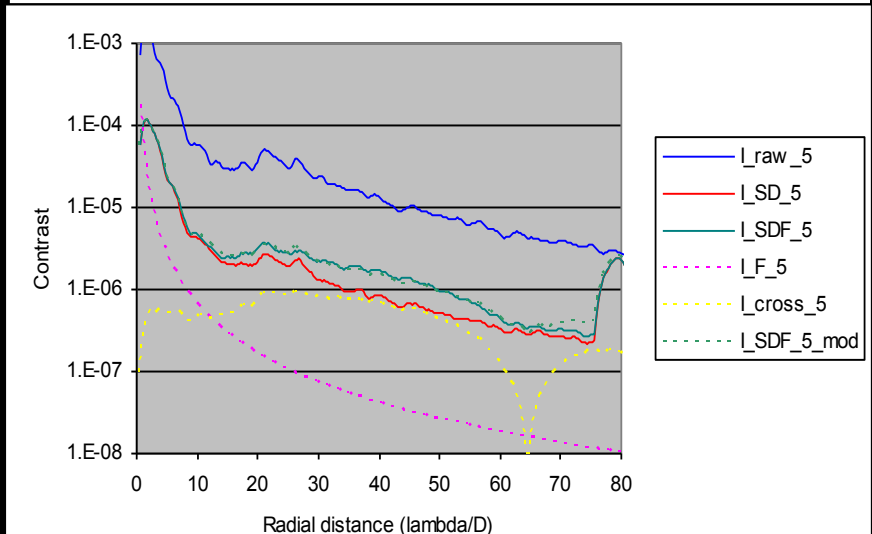
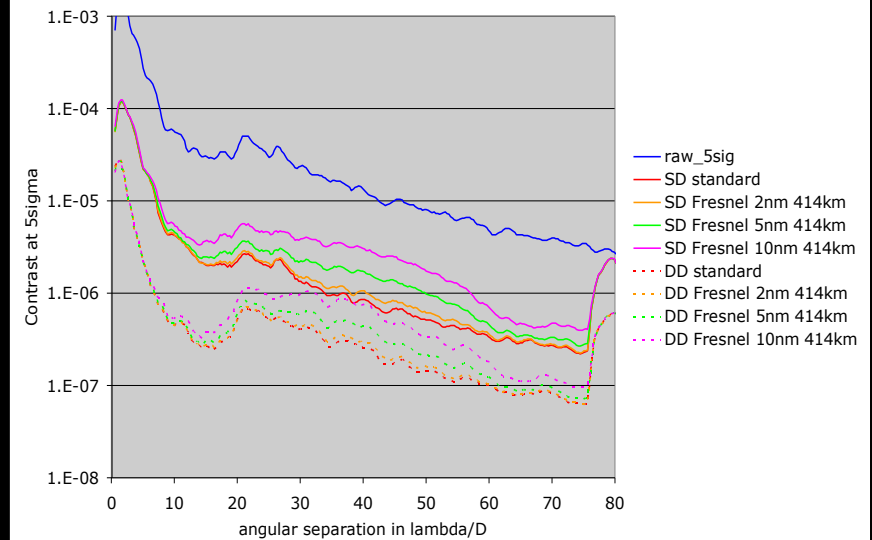
$$I_{SD}^F = I_{SD} + \sqrt{I_{Raw}I_{OutPup}} \sin(\pi \Delta N_T)$$

- The sin term includes the differential Talbot order:

$$\Delta N_T = \frac{h}{L_T} \frac{\Delta \lambda}{\lambda}$$

$$L_T = \frac{2\Lambda^2}{\lambda} = \frac{2(D/f)^2}{\lambda}$$

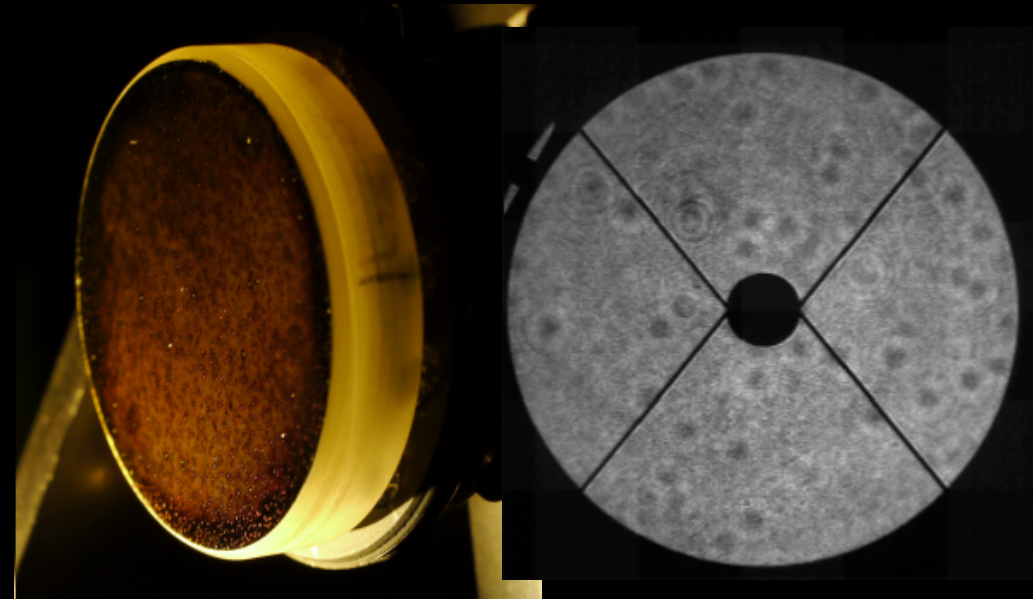
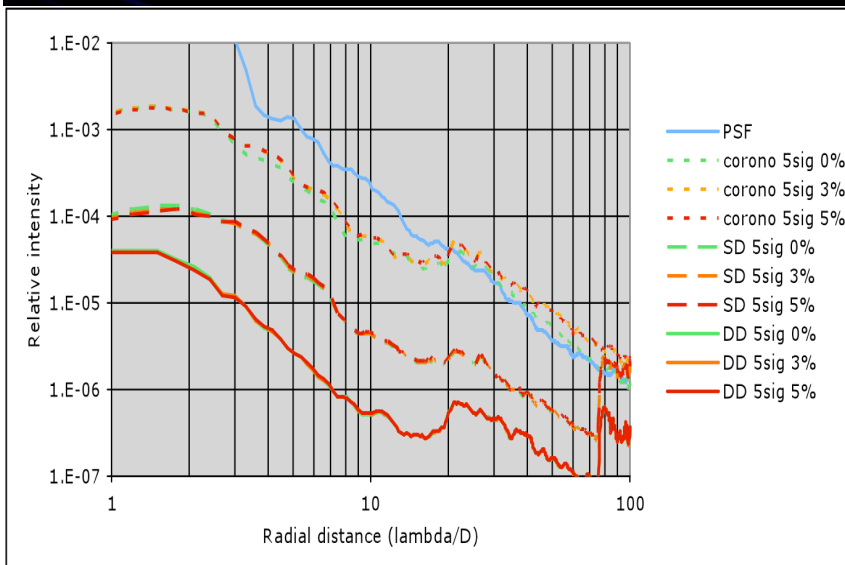
- "Bulge" appears, peaking at $\Delta N_T = 0.5$
- CAOS simulations confirm this simple model
 - To avoid the bulge within the AO corrected area, need $h < 2000\text{km}$
 - Most critical surface in SPHERE is DTTS BS: $h = 420\text{km}$
 - Specified and manufactured to 5nm rms



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Transmission non-uniformity

- By simulations established that this is not very critical
- Assume a total budget of 5% rms variation
 - Insignificant performance reduction
 - Allocate 0.5% to each instrument optics (not measured)
 - Leave 4.5% to the telescope optics (not measured)
- Should be OK
- ... if it wasn't for degradation of mirrors occurring since a few weeks





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Conclusions

- WFE budget elaborated in terms of PSD
 - Accounts for numerous instrumental effects such as beam shift etc
 - As-built budgets are conforming with design
 - Differential aberrations at goal spec
- Feeds into performance simulations
 - CAOS software package
 - Module for Fresnel effect implemented
- Predicted double difference performance in the NIR compatible with goal specs
 - 10^{-5} at 0.1"
 - $5 \cdot 10^{-7}$ at 0.5"
- Main current high-risk item: Mirror coatings

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