

Kinetic Theory

Distribution functions

A distribution function $f(\vec{x}, \vec{u}, t)$ is used for the description at a microscopic level. It is a phase space distribution function: $(\vec{x}, \vec{v}) \in \mathbb{R}^6$

Examples:

$f \equiv$ mass density: $\int_{\mathbb{R}^3} \int_{\mathbb{R}^3} f(\vec{x}, \vec{u}, t) d^3x d^3u = M$

$f \equiv$ probability density: $\int_{\mathbb{R}^3} \int_{\mathbb{R}^3} f(\vec{x}, \vec{u}, t) d^3x d^3u = 1$

A particle-by-particle description is not possible, instead we use a statistical description with the distributions.

Definition of $f(\vec{x}, \vec{u}, t)$: Average number of particles contained at time t in a volume element d^3x about \vec{x} and a velocity-space element d^3u about \vec{u} is $f d^3x d^3u$.
Furthermore we demand:

- $f \geq 0$ everywhere
- $u_i \rightarrow \infty, f \rightarrow 0$ sufficiently rapidly so that a finite amount of particles has a finite energy.

Moments

Generally: $Q(\vec{x}, t) = \int_{\mathbb{R}^3} f(\vec{x}, \vec{u}, t) q(\vec{u}) d^3u$

p -th moment: $Q_p(\vec{x}, t) = \int_{\mathbb{R}^3} f(\vec{x}, \vec{u}, t) u^p d^3u$

0-th moment: $Q_0 = \int_{\mathbb{R}^3} f(\vec{x}, \vec{u}, t) d^3u = n(\vec{x}, t)$ number density

1-st moment: $Q_1 = \int_{\mathbb{R}^3} f \vec{u} d^3u = n(\vec{x}, t) \cdot \vec{v}(\vec{x}, t)$ average velocity

2-nd moment: $E(\vec{x}, t) = \frac{1}{2} m \cdot Q_2$

Binary Collisions

The wave packets of particles are highly localised. To a very high degree of approximation, we can consider the gas to be a collection of classical point particles. We can describe the motion of a (electrically not charged) particle as a ^{sequence of} straight lines, each interrupted by a brief collision with another particle. Because the probability of collisions is small, we neglect the possibility of a collision of 3 or more particles simultaneously, and consider only binary collisions.

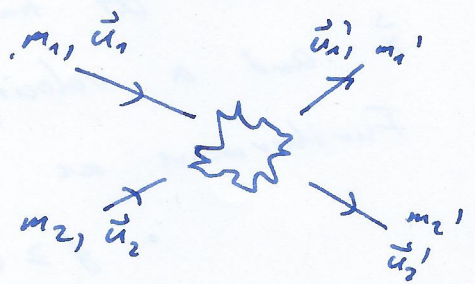
Binary collisions are collisions between two particles. They conserve energy and are characterised by a collision cross section.

Conserved quantities:

Mass: $M = m_1 + m_2 = m_1' + m_2'$

Momentum: $m_1 \vec{u}_1 + m_2 \vec{u}_2 = m_1 \vec{u}_1' + m_2 \vec{u}_2'$

Energy: $\frac{1}{2} m_1 u_1^2 + \frac{1}{2} m_2 u_2^2 = \frac{1}{2} m_1 u_1'^2 + \frac{1}{2} m_2 u_2'^2$



Now define: $\vec{V} = \frac{1}{M} (m_1 \vec{u}_1 + m_2 \vec{u}_2)$ Com-velocity

$\vec{v} = \vec{u}_1 - \vec{u}_2$ relative velocity

$\mu = \frac{m_1 m_2}{m_1 + m_2}$ reduced mass

Then: $E = \frac{1}{2} m_1 u_1^2 + \frac{1}{2} m_2 u_2^2 = \frac{1}{2} M V^2 + \frac{1}{2} \mu v^2$

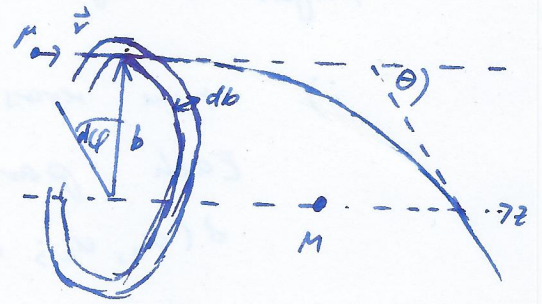
Energy conservation: $E = E' \Rightarrow \|V\| = \|V'\|$

\Rightarrow The relative velocity of the two particles only changes the direction after a collision!

Cross sections

(Differential cross sections)

Choose a particle to act as a collision center and bombard it with a flux of particles.



The rate of collisions R_1 that have the impact parameter in the range $(b, b+db)$ within an increment of $d\phi$ is $j \cdot b \cdot db \cdot d\phi$, where j is the incident flux.

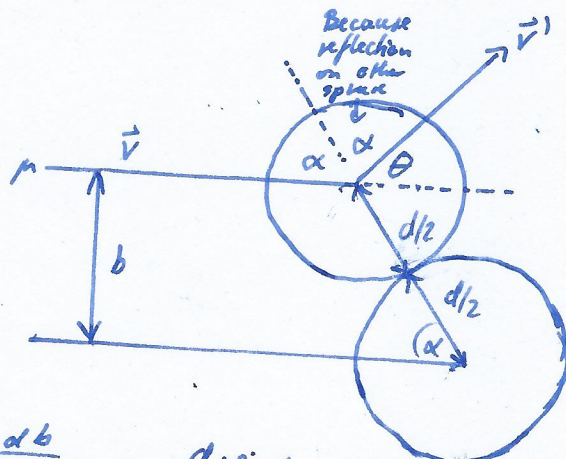
We can also assign the process a differential cross section σ defined as the rate at which particles are scattered out of the incident beam into an increment of solid angle $d\Omega$ around some direction \hat{u} , specified by the angles (θ, ϕ) . The rate will be $R_2 = j \cdot \sigma \cdot d\Omega$.

But because such a collision must have a unique solution, we can relate those two rates: $R_1 = R_2$ defines σ . With $d\Omega = \sin\theta \cdot d\theta \cdot d\phi$, we get:

$$\sigma = \frac{b}{\sin\theta} \frac{db}{d\theta}$$

differential cross section

For two rigid spheres of diameter d , we can see that $b = 2 \cdot \frac{d}{2} \cdot \sin(\alpha) = d \sin\alpha$



and $\theta = \pi - 2\alpha$.

This gives us:
$$\sigma = \frac{b}{\sin\theta} \frac{db}{d\theta} = \frac{d \cdot \sin\alpha}{\sin(\pi - 2\alpha)} \frac{db}{d\alpha} \frac{d\alpha}{d\theta} = \frac{d \cdot \sin\alpha}{2 \sin\alpha \cos\alpha} \cdot d \cdot \cos\alpha \cdot \frac{1}{2} = \frac{1}{4} d^2$$

Then the total cross section is:
$$\sigma_{tot} = \int \sigma \cdot d\Omega = 4\pi \sigma = \pi d^2$$

Properties of differential cross sections:

i) time reversal invariance

Each particle must retrace its original trajectory:

$$\delta(u_1, u_2; u_1', u_2') = \delta(-u_1', -u_2'; -u_1, -u_2)$$

ii) rotation / reflection invariance

The collision only depends on the magnitude and the relative velocities

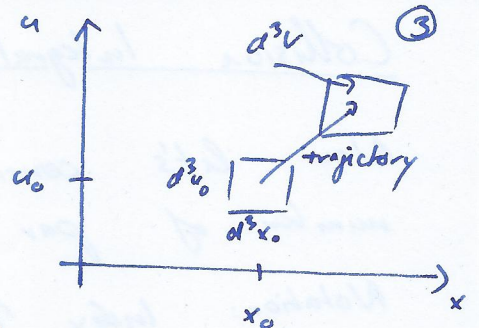
iii) reverse collision invariance

exchange $u_1, u_2 \leftrightarrow u_1', u_2'$ (time reversal + 180° rotation)



Boltzmann Equation

Vlasov equation



Interpret the timely evolution of a phase-space element as a coordinate transformation.

Neglecting second order terms, we have: $\begin{cases} \vec{x} \approx \vec{x}_0 + \vec{u}_0 dt \\ \vec{u} \approx \vec{u}_0 + \vec{a} dt \end{cases}$
 (assuming $\frac{\partial a}{\partial u} = 0$). The phase-space element $d^3x_0 d^3u_0$ "evolves" to $d^3x d^3u$.

The jacobian of the transformation gives:

$$J = \begin{vmatrix} \partial x / \partial x_0 & \partial x / \partial u_0 \\ \partial u / \partial x_0 & \partial u / \partial u_0 \end{vmatrix} = \begin{vmatrix} 1 & dt \\ \frac{\partial a}{\partial x} dt & 1 \end{vmatrix} = 1 + \frac{\partial a}{\partial x} dt^2 \approx 1$$

\Rightarrow The volume element is conserved

Let δN_0 be the number of particles in dV_0 . Assuming we have no collisions that might remove or add particles, then $\Rightarrow \delta N_0 \stackrel{!}{=} \delta N$

$$\Rightarrow \delta N_0 = f(\vec{x}_0, \vec{u}_0, t) d^3x_0 d^3u_0 \stackrel{!}{=} f(\vec{x}_0 + \vec{u}_0 dt, \vec{u}_0 + \vec{a} dt, t_0 + dt) d^3x d^3u$$

Now as shown, $d^3x d^3u = d^3x_0 d^3u_0$

$$\Rightarrow f(\vec{x}_0, \vec{u}_0, t) = f(\vec{x}_0 + \vec{u}_0 dt, \vec{u}_0 + \vec{a} dt, t_0 + dt)$$

\Rightarrow The distribution function is the same for all particles everywhere

\Rightarrow Vlasov's equation: Expand to first order in dt .

$$\boxed{\frac{\partial f}{\partial t} + \vec{v} \frac{\partial f}{\partial \vec{x}} + \vec{a} \frac{\partial f}{\partial \vec{u}} = 0} = \frac{Df}{Dt}$$

$$= \frac{\partial f}{\partial t} dt + \frac{\partial f}{\partial \vec{x}} \frac{\partial \vec{x}}{\partial t} dt + \frac{\partial f}{\partial \vec{u}} \frac{\partial \vec{u}}{\partial t} dt \quad [\text{first order expansion}]$$

Collision Integral

Now let's consider the case where binary collisions change the number of particles of a phase-space element.

Notation: Index 2: Target particles; Index 1: collider particles

~~Suppose only 1 outward collide particle interacts with the particles in our phase space element dV_2 . In that case, the rate of change of the number of particles is~~

The change in particle numbers in the volume element dV_2 can be described as follows: (v : relative velocity)

$$\begin{aligned} \delta N_2 &= \# \text{ particles inside} \cdot [\# \text{ particles incoming} \cdot \text{probab. to collide}] \\ &= \int_2 d^3v \cdot \left[\int_1 (\sigma d\Omega) \cdot v \cdot dt \right] \end{aligned}$$

$$= \int_1 \int_2 \sigma v d^3v dt d\Omega$$

Volume element containing probability of collisions through cross sections

$$\Rightarrow \boxed{\frac{\delta N_2}{dt} = \int_1 \int_2 \sigma v d^3v d\Omega}$$

for outgoing collisions.

By demanding the process to be reversible, using the same arguments, we can write for the incoming collisions:

$$\boxed{\frac{\delta N_1}{dt} = \int_1' \int_2' \sigma v d\Omega d^3v}$$

(also using $v' = v$)

With these two expressions, we find the collision integral:

$$d\left(\frac{Df}{Dt}\right)_{\text{coll}} = \text{sources} - \text{sinks} = \frac{\delta N_2}{dt} - \frac{\delta N_1}{dt} = [\int_1' \int_2' - \int_1 \int_2] \sigma v d\Omega d^3v$$

$$\Rightarrow \boxed{\left(\frac{Df}{Dt}\right)_{\text{coll}} = \iint [\int_1' \int_2' - \int_1 \int_2] \sigma v d\Omega d^3v}$$

Collision Invariants

Invariants of the collision integral are also invariants of the Boltzmann equation; Finding them gives us conservation laws.

A moment $Q(\vec{u}_i)$ is an invariant if:

$$I(\vec{x}, t) \equiv \iiint Q(\vec{u}_i) [(f_1' f_2' - f_1 f_2) \sigma v d\Omega d^3v_2] d^3v_1 \stackrel{!}{=} 0 \Rightarrow Q \text{ invariant}$$

The particles must be interchangeable:

$$\Rightarrow I(\vec{x}, t) = \iiint Q(\vec{u}_2) [(f_1' f_2' - f_1 f_2) \sigma v d\Omega d^3v_1] d^3v_2$$

$$\Rightarrow I = \frac{1}{2}(I+I) = \frac{1}{2} \iiint [Q(\vec{u}_1) + Q(\vec{u}_2)] [(f_1' f_2' - f_1 f_2) \sigma v d\Omega d^3v_1] d^3v_2$$

Reverse collisions also have to hold:

$$I = \frac{1}{2} \iiint [Q(\vec{u}_1') + Q(\vec{u}_2')] [f_1 f_2 - f_1' f_2'] \sigma v d\Omega d^3v_1 d^3v_2$$
$$= \frac{1}{2}(I+I)$$

$$= \frac{1}{4} \iiint [Q(\vec{u}_1) + Q(\vec{u}_2) - Q(\vec{u}_1') - Q(\vec{u}_2')] [f_1' f_2' - f_1 f_2] \sigma v d\Omega d^3v_1 d^3v_2$$

With $I \equiv 0 \Rightarrow Q(\vec{u}_1) + Q(\vec{u}_2) = Q(\vec{u}_1') + Q(\vec{u}_2')$

Equilibria

LTE: Internal state of a system in which over a timescale of interest no macroscopic flows of matter or energy are present.

Detailed Balance: At equilibrium, each elementary process (= collisions) is balanced by its reverse process.

LTE \Rightarrow Detailed Balance, but not the other way around!

In equilibrium: (Global Thermodynamic equilibrium)

$$\frac{\partial f}{\partial t} = 0$$

static

$$\frac{\partial f}{\partial \vec{x}} = 0$$

Uniform in space

$$\frac{\partial f}{\partial \vec{u}} = 0$$

no perturbations ($\bar{a} = 0$)

For local: $\left(\frac{\partial f}{\partial t}\right)_{\text{coll}} = 0$ suffices.

Other simplifications:

$$\vec{v} = 0$$

static

$$\ddot{a} = 0$$

isolated

Maxwell-Boltzmann distribution

The Maxwell-Boltzmann distribution is a distribution for a system in LTE.

Thus demanding detailed balance: $f_1' f_2' = f_1 f_2$

$$\Rightarrow \ln f_1' + \ln f_2' = \ln f_1 + \ln f_2$$

\Rightarrow If $\ln f_i = Q_i = \alpha$ an invariant moment, the condition for detailed balance is satisfied and we get conservation laws.

Ausatz: We have 3 collision invariants ($m, m\vec{v}, \frac{1}{2}mv^2$) and 3 equations; so f must be a function of those moments so the equations won't be overdetermined

$$\Rightarrow \ln f_0 = \alpha + \vec{\beta} \cdot \vec{u} + \gamma \frac{1}{2} u^2$$

$$\Rightarrow f_0 = \frac{n(\vec{x}, t)}{(2\pi\sigma^2)^{3/2}} e^{-1/2 [\vec{v} - \vec{u}(\vec{x}, t)]^2 / \sigma^2}$$

- With:
- \vec{u} : particle density
 - \vec{v} : bulk velocity
 - \vec{u} : particle velocity
 - σ^2 : $\frac{k_B T}{m}$ velocity dispersion
 - Statistical dispersion of velocities about the mean velocity.

Properties:

$$\int f_0 d\vec{v} = 1$$

$$\int f_0(\vec{v}) \cdot \vec{v} d\vec{v} = 0$$

$$\int f_0 v^2 d\vec{v} = \sigma^2$$

f_0 even, v odd, together odd $\Rightarrow 0$

Collision Time, Mean Free Path

Consider two species of particles. The collision rate between them can be approximated with:

$$\begin{aligned} C_{12} &= \# \text{ species 1} \cdot \# \text{ species 2} \cdot \text{prob. to collide / dt} \\ &= \frac{\delta N}{\delta t} = \iint n_1 f_1 f_2 \delta v \delta t d^3 v_1 d^3 v_2 / \delta t \\ &= \frac{n_1 \cdot n_2 \cdot \langle \delta v \rangle \delta t}{\delta t} = n_1 n_2 \langle \delta v \rangle \end{aligned}$$

The collision time is defined for a species as the reciprocal of the collision rate:

$$\tau_{\text{coll}} = \frac{n_1}{C_{12}} = \frac{1}{n_2 \langle \delta v \rangle}$$

Mean free path: Average length between two collisions

$$\lambda = \langle v \rangle \cdot \tau_{\text{coll}} = \frac{1}{n_2 \delta} \quad (\text{independent of } T!)$$

For rigid spheres: $\delta = \delta_0 = 10^{-15} \text{ cm}^{-2}$
for $T < 10^3 - 10^4 \text{ K}$

$$\begin{aligned} \langle v \rangle &\approx \delta^2 \quad (\text{velocity dispersion}) \\ &\text{in COM-frame.} \\ &= \sqrt{\frac{k_B T}{\mu}} \end{aligned}$$

Validity of MB:

Define scale height of parameters $p = n, v, T$: $h(p) \equiv \left| \frac{1}{p} \nabla p \right|$
If the spatial gradients of these parameters is small enough, the system can be considered locally uniform and thus in LTE.

$$\Rightarrow h(p) \equiv \left| \frac{1}{p} \nabla p \right| < 1/2$$

Moments of the Boltzmann equation

(6)

Take Boltzmann equation: $\frac{\partial f}{\partial t} + \vec{v} \frac{\partial f}{\partial \vec{x}} + \vec{a} \frac{\partial f}{\partial \vec{v}} = \left(\frac{Df}{Dt} \right)_{\text{coll}}$

If you multiply both sides with a moment ($m, m\vec{v}, \frac{1}{2}m\vec{v}^2$) and integrate over all space, we can derive for each moment a conservation law. (Because $\int \left(\frac{Df}{Dt} \right)_{\text{coll}} \cdot Q d^3v = 0$ as shown before; moments are collision invariants)

Remember: • t, \vec{x}, \vec{v} are independent variables! (change the order as you please)

• f sinks to 0 more rapidly than any power law (definition of distribution): $\lim_{\alpha \rightarrow \infty} \alpha^n f(\alpha) = 0 \forall \alpha, n$

• $\vec{a} = \vec{a}(\vec{x})$

1) Mass conservation

$$\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \langle \vec{v} \rangle) = 0$$

2) Momentum conservation

$$\frac{\partial}{\partial t} (\rho \vec{u}) + \vec{\nabla} \cdot (\rho \vec{u} \otimes \vec{u} + \underline{\underline{P}}) = \rho \vec{a}(\vec{x})$$

with $(\vec{u} \otimes \vec{u})_{ij} = u_i u_j$

$$P_{ij} = \int_{\mathbb{R}^3} m f w_i w_j d^3v \quad \text{Pressure tensor}$$

3) Energy conservation

$$\frac{\partial E}{\partial t} + \vec{\nabla} \cdot (E \vec{u} + \underline{\underline{P}} \vec{u} + \vec{Q}) = \rho \vec{a} \cdot \vec{u}$$

with $\vec{Q} = \int \frac{1}{2} m w^2 \vec{w} f d^3v$ heat flux

Euler Equations

The Euler equations are the moments of the Boltzmann equation where $f = f_0 = f_{\text{Maxwell-Boltzmann}}$.

In this case, \bar{P} and \bar{Q} simplify:

$$P_{ij} = \int_{\mathbb{R}^3} m w_i w_j f d^3v = \int_{\mathbb{R}^3} m w_i w_j n g(w_x) g(w_y) g(w_z) d^3v.$$

For $i \neq j$: Odd power of $w_i \Rightarrow$ Integral = 0 $g(w_i)$: 1D-gauss

$\Rightarrow P_{ij}$ is diagonal $\rightarrow \bar{P} = P \mathbb{1}$

For $i=j$:

$$P_{ii} = \int_{\mathbb{R}^3} m w_i^2 n g(w_x) g(w_y) g(w_z) d^3v = 1 \cdot 1 \cdot 3 \cdot \sigma^2$$

And for \bar{Q} : $\bar{Q} = \int \frac{1}{2} m w^2 \vec{u} f_0 d^3v = 0$ (again even-odd)

This gives us the Euler equations:

$$\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \vec{u}) = 0$$

$$\frac{D\rho}{Dt} = -\rho \vec{\nabla} \cdot \vec{u}$$

$$\frac{\partial}{\partial t} (\rho \vec{u}) + \vec{\nabla} \cdot (\rho \vec{u} \otimes \vec{u} + P \mathbb{1}) = \rho \vec{a}$$

$$\frac{D\vec{u}}{Dt} = -\frac{1}{\rho} \nabla P + \vec{a}$$

$$\frac{\partial E}{\partial t} + \vec{\nabla} \cdot (E + P) \vec{u} = \rho \vec{a} \cdot \vec{u}$$

$$\frac{De}{Dt} = -\frac{1}{\rho} P \vec{\nabla} \cdot \vec{u}$$

$$E = \frac{1}{2} \rho u^2 + e$$

$$e = \int \frac{1}{2} m w^2 f d^3v = \frac{1}{2} T_V(P) = (\gamma+1) P \quad \text{internal energy}$$

Quantum Physics and Kinetic Theory

Typical size of quantum cell: $d^6V = d^3r d^3v \approx h^3$

Occupation number N : Number of particles per cell

$$N \approx f h^3$$

Types of particles:

Fermions: $N \leq 1$ (Pauli exclusion)

Bosons: $N \gg 1$

We need to add a suppression/enhancement factor into the integrand of the collision integral:

$$\frac{\delta N_1}{\delta t} = \int_1 \int_2 \sigma v (1 \pm N_1')(1 \pm N_2')$$

← depends on the situation of ~~the~~ where the particles will land in!

$$\frac{\delta N_2}{\delta t} = \int_1 \int_2' \sigma v (1 \pm N_1)(1 \pm N_2)$$

+ for Bosons.

These terms give us the statistics:

Bose-Einstein:
$$f_{BE} = \frac{1}{h^3} \frac{1}{\Omega e^{(E-\mu)/k_B T}}$$

Fermi-Dirac:
$$f_{FD} = \frac{1}{h^3} \frac{1}{1 + e^{(E-\mu)/k_B T}}$$

Equations of State

EOS relate state quantities such as pressure, density and temperature.

Isothermal EOS: $P = a^2 \rho$

$$a^2 = c^2 = \frac{k_B T_0}{m} \quad (\text{ideal gas eqn})$$

adiabatic stuff: $\gamma = \frac{C_p}{C_v} = \frac{f+2}{f}$ (ideal gas)

$$P = (\gamma - 1) \rho E = (\gamma - 1) \rho e$$

$$E = \rho e + \frac{1}{2} \rho v^2$$

$$e = \frac{U}{V} = \frac{N k_B T}{V}$$

Polytropic EOS: $P = P_0 \left(\frac{\rho}{\rho_0} \right)^\Gamma$

Degenerate (for very high densities, where QM is important again)

For low temperatures, depends only on S (Pauli pushes)

Derivation: Isotropic stress tensor, assume radial symmetry

Approximate $E \approx \frac{\rho^2}{2m}$, $w \approx \frac{p}{m}$

Take Fermi distribution:

with $\mu = E_F + mc^2$ $f = \frac{g}{\Omega} = \frac{1}{1 + e^{-(E-\mu)/k_B T}}$

Degenerate Equations of State

①

fermi-dirac distribution: $f(E) = \frac{g}{h^3} \frac{1}{e^{(E-E_F)/k_B T} + 1}$

number density: $n = \int f d^3 p = 4\pi \int f p^2 dp$

Degeneracy: $f(E > E_F) \approx 0$ For $k_B T \ll E_F$

Pressure for isotropic gas:

$$P_{zz} = \int m f v_z v_z d^3 p = \int v_z p_z f d^3 p =$$

$$= \int v \cos \theta p \cos \theta f p^2 \sin \theta d\theta d\phi dp$$

$$= \int v p f p^2 \sin \theta \cos^2 \theta d\theta d\phi dp$$

Now use: $\int \cos^2 \theta \sin \theta d\theta = [-\cos \theta \cos^2 \theta]_0^\pi - 2 \int \cos^2 \theta \sin \theta d\theta$

$$\Rightarrow 3 \int \cos^2 \theta \sin \theta d\theta = [1 + 1] = 2$$

$$\Rightarrow \int \cos^2 \theta \sin \theta d\theta = 2/3$$

$$\begin{aligned} \int u' v' &= uv - \int u v' \\ u' &= \sin \quad v = \cos^2 \\ u &= -\cos \quad v' = 2 \cos \sin \end{aligned}$$

$$= \frac{2}{3} \cdot 2\pi \int v p f p^2 dp = \boxed{\frac{1}{3} \int v p f 4\pi p^2 dp}$$

1) Relativistic Regime

$$E = \sqrt{m^2 c^2 + p^2 c^2} \approx pc$$

$$\hookrightarrow f(E) = f(p) = \frac{g}{h^3} \frac{1}{e^{(p-p_F)c/k_B T} + 1}$$

a) Cold case: $k_B T \ll E_F$

for $p < p_F$: $e^{(p-p_F)c/k_B T} \approx 0$

$$\hookrightarrow f(p) \approx \frac{g}{h^3}$$

$$\Rightarrow n = \int_0^{p_F} f d^3 p = 4\pi \int_0^{p_F} \frac{g}{h^3} p^2 dp = \boxed{\frac{4\pi g}{3 h^3} p_F^3}$$

$$P = \frac{4\pi}{3} \int_0^{\infty} f \cdot v \cdot p^3 dp \stackrel{v=c}{=} \frac{4\pi}{3} \int_0^{p_F} \frac{4\pi g}{h^3} \cdot c \cdot p^3 dp$$

$$= \frac{4\pi^2 g}{3 h^3} c p_F^4$$

2) Non-Relativistic Regime

Same arguments: $f \approx \frac{g}{h^3}$

$$\rightarrow n = \int_0^{p_F} 4\pi f p^2 dp = \frac{4\pi}{3} \frac{g}{h^3} p_F^3$$

$$P = \frac{4\pi}{3} \int_0^{p_F} f p v p^2 dp \stackrel{v=p/m}{=}$$

$$= \frac{4\pi}{3} \int_0^{p_F} \frac{g}{h^3} \frac{p^4}{m} dp$$

$$= \frac{4\pi}{15} \frac{g}{h^3} \frac{1}{m} p_F^5$$

What if non-degenerate? $E - E_F \gg k_B T$?

→ exponential term of FD-distribution is dominant:

$$f \approx \frac{g}{h^3} e^{-(E - \mu)/k_B T} \stackrel{E = mc^2 + p^2/2m}{=} \frac{g}{h^3} e^{-(mc^2 + p^2/2m)/k_B T}$$

$$= \frac{g}{h^3} e^{-mc^2/k_B T} e^{-p^2/2mk_B T} = \frac{g}{h^3} e^{-mc^2/k_B T} e^{-\frac{v^2}{2k_B T/m}}$$

→ distribution approximates Maxwell-Boltzmann distribution again (non-relativistic)

Boltzmann's H-Theorem

A gas kinetic formulation of the second law of thermodynamics. (Entropy) H can only decrease over time.

Consider an isolated ($\vec{a}=0$) uniform ($\frac{\partial f}{\partial x_i} = 0$) medium.

Then define $H = \int_{\mathbb{R}^3} f(\vec{v}, t) \ln(f(\vec{v}, t)) d^3v$

$$\begin{aligned} L) \frac{dH}{dt} &= \int_{\mathbb{R}^3} \frac{d}{dt} [f \ln(f)] d^3u_1 = \\ &= \int d^3u_1 \left[\frac{df}{dt} \ln(f) + f \cdot \frac{d \ln(f)}{dt} \right] d^3u_1 \\ &= \int d^3u_1 \left[\left(\frac{\partial f}{\partial t} + \underbrace{\frac{\partial f}{\partial x_i} \cdot \vec{v} + \frac{\partial f}{\partial v_i} \vec{a}}_{=0} \right) \ln f + f \cdot \frac{1}{f} \left(\frac{\partial f}{\partial t} + 0 + 0 \right) \right] d^3u_1 \\ &= \int d^3u_1 (1 + \ln f) \frac{\partial f}{\partial t} \quad [1] \end{aligned}$$

On the other hand, consider the Boltzmann equation in this case:

$$\frac{\partial f}{\partial t} + \underbrace{\vec{v} \frac{\partial f}{\partial x_i} + \vec{a} \frac{\partial f}{\partial v_i}}_{=0} = \frac{\partial f}{\partial t} = \left(\frac{Df}{Dt} \right)_{\text{coll}} = \iint (f_1' f_2' - f_1 f_2) v \, d\Omega \, d^3u_1 \, d^3u_2$$

$$\Rightarrow \frac{\partial H}{\partial t} = \iiint \underbrace{[\ln f + 1]}_Q (f_1' f_2' - f_1 f_2) v \, d\Omega \, d^3u_1 \, d^3u_2$$

We see that we can interpret $\ln f + 1$ as a collision invariant Q

By demanding that collisions can be inverted in time ($Q(u_1) = Q(u_2)$), then $\frac{\partial H}{\partial t} = \frac{1}{2} \left(\frac{\partial H}{\partial t} + \frac{\partial H}{\partial t} \text{reversed} \right)$ and then applying the demand for inverse collisions ($\cdot \rightarrow -\cdot$) we obtain:

$$\frac{\partial H}{\partial t} = \frac{1}{2} \iiint [\ln(f_1' f_2') - \ln(f_1 f_2)] (f_1' f_2' - f_1 f_2) v \, d\Omega \, d^3u_1 \, d^3u_2$$

$$\text{or: } \frac{dH}{dt} = -\frac{1}{4} \underbrace{\ln\left(\frac{f_1' f_2'}{f_1 f_2}\right)}_a \underbrace{(f_1' f_2' - f_1 f_2)}_b v_1 v_2 d^3 u_1 d^3 u_2$$

Now if $(f_1 f_2) < (f_1' f_2') : a > 0, b > 0 \Rightarrow \frac{dH}{dt} \leq 0$
 $(f_1 f_2) > (f_1' f_2') : a < 0, b < 0 \Rightarrow \frac{dH}{dt} \leq 0$

$$\Rightarrow \frac{dH}{dt} \leq 0.$$

Now look at eq [1]. In an LTE, we must have $\frac{\partial A}{\partial t} = 0 \Rightarrow \frac{dH}{dt} = 0.$

That means that in LTE, we have $f_1' f_2' = f_1 f_2$
 \hookrightarrow We get MB distributions.

H must have a lower boundary because systems must have finite energy.

\Rightarrow If the system is in LTE, we have detailed balance.

Chapman - Enskog theory

= a perturbative approach for dealing with systems in non-LTE conditions.

Ansatz: $f = f_{M0} + \delta f, \quad |\delta f| \ll |f_{M0}|$

Collision time approximation: $\frac{\partial f}{\partial t} \sim \vec{u} \cdot \nabla f \approx -\frac{\delta f}{\tau_{coll}}$

Results: Viscosity (= non-diagonal elements of pressure tensor) and heat flux re-enter the equations

Heat conduction coefficient:

Assume $\rho = \rho_0, \quad \vec{v} = 0$

Then $\frac{\partial E}{\partial t} = -\nabla \cdot (\kappa \vec{\nabla} T) = -\vec{\nabla} \cdot \vec{Q} = -\kappa \Delta T$

with $E = \frac{1}{2} n k_B T: \quad \frac{\partial T}{\partial t} = \frac{-\kappa}{\frac{1}{2} n k_B} \Delta T = \nu \Delta T$

Dimensional analysis:

$[w] = m^2/s \rightarrow$ Ansatz $w = \sigma \cdot \lambda \quad \sigma: \text{vel. disp.}$

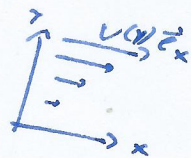
with $\lambda = \sigma \tau_{coll} \rightarrow w = \sigma^2 \tau_{coll} = \frac{-\kappa}{\frac{1}{2} n k_B}$

$\Rightarrow \kappa = -\frac{1}{2} n k_B \sigma^2 \tau_{coll} = -\frac{1}{2} \frac{\rho}{m} k_B T \sigma^2 \tau_{coll} = \left| -\frac{1}{2} \frac{\rho \sigma^4}{T} \tau_{coll} \right|$

Viscosity coefficient

Viscosity tensor: $D_{ij} = \frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} - \frac{2}{3} (\vec{\nabla} \cdot \vec{v}) \delta_{ij}$

Gives us: $\frac{\partial \vec{v}}{\partial t} = \frac{\nu}{\rho} \frac{\partial^2 \vec{u}}{\partial x^2} = \nu \frac{\partial^2 \vec{u}}{\partial x^2}$



Dimensional analysis: $[w] = \frac{m^2}{s} \rightarrow w = \sigma^2 \tau_{coll} (= \sigma \lambda)$

$w = \sigma^2 \tau_{coll} = \frac{\nu}{\rho} \Rightarrow \left| \nu = \rho \sigma^2 \tau_{coll} \right|$

$\kappa \propto T^{1/2} m^{-1/2}$: small particles dominate

$\nu \propto T^{1/2} m^{1/2}$: large particles dominate

Coulomb gas

Problem: $\frac{1}{r}$ potential $\neq 0$ for very large distances.

→ Add cut-off when you consider plasma to be neutral again.

Get impact parameter for 90° deflection: (= must stop at center completely) $\Rightarrow \frac{1}{2} m v^2 = \frac{e^2}{b_{90}} \Rightarrow b_{90} = \frac{2e^2}{m v^2}$

Cross section rigid spheres:

$$\sigma_{ca} = \pi b_{90}^2 = \frac{4e^4}{m^2 v^4} = \frac{4e^4}{(k_B T/m)^2} \times \ln \Lambda$$

constant logarithm
for cut off

Vinial Theorem

Scalar moment of inertia: $I(t) = \int_{V(t)} \rho(x, t) x^2 d^3x$

Reynold's transport theorem: With $I = \int_{V(t)} \alpha d^3x$

$$\dot{I} = \int_{V(t)} \left[\frac{\partial \alpha}{\partial t} + \nabla \cdot (\alpha \cdot \vec{v}) \right] d^3x$$

Vinial theorem:

$$\begin{aligned} \frac{1}{2} \dot{I}(t) &= \int \rho \vec{v} d^3x + \int 3P d^3x + \int \rho \vec{x} \cdot \vec{g} d^3x - \int_S P \vec{x} \cdot \vec{n} dS \\ &= 2K + V - S \end{aligned}$$

For isolated objects: $S=0$

Simple solutions:

Poisson equ: $\Delta \phi = 4\pi G \rho$; $\vec{\nabla} \phi = -\vec{g}$

$$\rightarrow \vec{g}(r) = -\frac{GM(r)}{r} \vec{e}_r$$

Static case: $\vec{u} = 0$

$$K = \int_V \left(\frac{1}{2} \rho u^2 + \frac{3}{2} P \right) d^3x = \frac{3}{2} P \frac{4\pi}{3} R^3$$

$$V = \int_V (\rho \vec{x} \cdot \vec{g}) d^3x = \int_0^R \rho g_r \cdot 4\pi r^2 dr = -\int \rho^2 G M$$

$$= \int \rho \left(-\frac{G \rho \frac{4\pi r^3}{3}}{r} \right) 4\pi r^2 dr = -G \rho^2 \frac{16\pi^2}{3} \int r^4 dr = -\frac{16\pi^2}{15} G \rho^2 R^5$$

$$S=0$$

With $2K + V = 0$

$$\Rightarrow 4\pi R^3 P = \frac{16\pi^2}{15} G \rho^2 R^5 \Rightarrow P = \frac{4\pi}{15} G \rho^2 R^2$$

Chose EOS: isothermal: $P = \frac{\rho h_0 T}{M}$

insert, Ulaula

Hydrostatic Equilibrium

Radial part of spherical Euler equations:

$$\frac{D_{ur}}{Dc} = \frac{u\phi^2}{r} - \frac{1}{s} \frac{\partial P}{\partial r} - \frac{\partial \phi}{\partial r}$$

For a system in global equilibrium: $\vec{u} = 0$

$$\Rightarrow \left[\frac{1}{s} \frac{\partial P}{\partial r} = -\frac{\partial \phi}{\partial r} \right]$$

Poisson equation: $\left[\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial \phi}{\partial r} \right) = 4\pi G \rho \right]$

Lane - Emden equation

Combination of Poisson + hydrost. equl, polytropic EOS
Can be nondimensionalized.

$$\rightarrow \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{1}{s} \frac{\partial P}{\partial r} \right) = -4\pi G \rho$$

Isothermal case: $\frac{1}{s} \frac{\partial P}{\partial r} = \frac{1}{s} a^2 \frac{\partial \rho}{\partial r} = -\frac{\partial \phi}{\partial r}$
 $\Rightarrow \rho = \rho_0 e^{-\phi/a^2}$

Singular solutions: $\rho = A r^{-\alpha}$ for isothermal

$$\frac{\partial \phi}{\partial r} = -a^2 \frac{1}{s} \frac{\partial \rho}{\partial r} = -a^2 \frac{1}{A r^{-\alpha}} \frac{\partial (A r^{-\alpha})}{\partial r} = a^2 \frac{\alpha}{r}$$

$$\rightarrow \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 a^2 \frac{\alpha}{r} \right) = 4\pi G A r^{-\alpha}$$

Accretion Disks

= Structures formed by diffused material in orbital motion around a central massive object. Disk spirals inward because of center object's gravitational force. \Rightarrow Dominant force contribution comes from central object.

Assume axisymmetry: $\vec{\nabla} \cdot \mathbf{A} = \frac{1}{r} \frac{\partial}{\partial r}(A_r r) + \frac{\partial A_z}{\partial z}$

\Rightarrow Mass conservation: $\frac{\partial \rho}{\partial t} + \frac{1}{r} \frac{\partial}{\partial r}(r v_r \rho) + \frac{\partial}{\partial z}(\rho v_z) = 0$

Get out z dependence: define surface mass density $\Sigma(r) = \int_{-\infty}^{\infty} \rho(r, z) dz$

Take Momentum Euler equations in (r, θ) :

i) $\rho \left[\frac{\partial v_r}{\partial t} + v_r \frac{\partial}{\partial r} v_r - \frac{v_\theta^2}{r} \right] = -\frac{\partial P}{\partial r} - \frac{\rho G M_*}{r^2}$

$\rightarrow \left[\Sigma \left[\frac{\partial v_r}{\partial t} + v_r \frac{\partial}{\partial r} v_r - \frac{v_\theta^2}{r} \right] = -\Sigma \frac{G M_*}{r^2} - \int dz \frac{\partial P}{\partial r} \right]$

ii) $\rho \left[\frac{\partial v_\theta}{\partial t} + v_r \frac{\partial}{\partial r} v_\theta + \frac{v_r v_\theta}{r} \right] = 0$: No forces in θ -direction!

$\rightarrow \left[\Sigma \left[\frac{\partial v_\theta}{\partial t} + v_r \frac{\partial v_\theta}{\partial r} + \frac{v_\theta v_r}{r} \right] = 0 \right]$

Accretion rate:

$\int \frac{\partial}{\partial z}(\rho v_z) dz = 0$ because $= \int \frac{\partial}{\partial z}(\rho v_z) dz = \rho v_z \Big|$

$\Rightarrow \dot{M} = \int \frac{\partial \rho}{\partial t} dV = \int d\theta \int dz \int r dr \frac{\partial \rho}{\partial t} = \int d\theta \int r dr \frac{1}{r} \frac{\partial}{\partial r}(r v_r \rho)$
 $= 2\pi r v_r \int \rho dz = 2\pi \Sigma r v_r$

$\boxed{\dot{M} = 2\pi \Sigma r v_r}$

Solutions:

1) Static equilibrium in radial direction

Set $v_r = 0$, $\frac{\partial}{\partial t}(\dots) = 0$, $\Rightarrow \dot{m} = 0$

$$\pi = \int_{-\infty}^{\infty} P dz$$

Only equation left:
$$\frac{v_0^2}{r} - \frac{GM}{r^2} = \frac{1}{\Sigma} \frac{\partial \pi}{\partial v}$$

Centrifugal equilibrium

Bondi Accretion

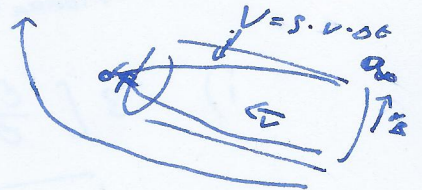
Very simplified model: Assume (wrongly) spherical accretion.

Ignore radiation and magnetic fields;

Assume infinite medium with known ρ_∞, a_∞ , with particles moving towards center.

Now determine which particles will fall in:

$$\frac{1}{2} m a_\infty^2 = \frac{GMm}{r_B} \rightarrow r_B \approx \frac{2GM}{a_\infty^2}$$



Then the accretion rate will be: $\dot{M} = \rho v 4\pi r^2 dr$

$$\dot{M}_B = \frac{dM}{dt} = \frac{[(\pi r_B^2) \cdot v \cdot dt] \cdot \rho}{dt} = \frac{4\pi G^2 M^2 a_\infty \rho_\infty}{a_\infty^4} = \frac{4\pi G^2 M^2 \rho_\infty}{a_\infty^3}$$